DOE/JPL-954977-78/1 Distribution Category UC-63

DRL-69-DRD-SE-2 Technical Report: MRI-269

# QUANTITATIVE ANALYSIS OF DEFECTS IN SILICON

Silicon Sheet Growth Development for the Large Area Silicon Sheet Task of the Low-Cost Solar Array Project

QUARTERLY PROGRESS REPORT NO. 4

by

R. Natesh J.M.Smith H.A.Oidwai

Covering the period 1 January 1979 to 31 March 1979

JPL Contract No. 954977

MATERIALS RESEARCH, INC. 790 East 700 South Street Centerville, Utah 84014 Phone: (801) 531-9600



The JPL Low-Cost Silicon Solar Array Project is sponsored by the U.S. Department of Energy and forms part of the Solar Photovoltaic Conversion Program to initiate a major effort toward the development of low-cost solar arrays. This work was performed for the Jet Propulsion Laboratory, California Institute of Technology, by agreement between NASA and DOE.

(NASA-CR-158738) QUANTITATIVE ANALYSIS OF N79-26492
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DEVELOPMENT FOR THE LARGE AREA SILICON SHEET
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#### TECHNICAL CONTENT STATEMENT

This report was prepared as an account of work sponsored by the United States Government. Neither the United States nor the United States Department of Energy, nor any of their employees, nor any of their contractors, subcontractors, or their employees, make any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights.

# NEW TECHNOLOGY

No new technology is reportable for the period covered by this report.

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#### SECTION I

# SUMMARY

This report describes the various steps involved in the chemical polishing and etching of Motorola silicon samples. Data on twins, dislocation pits, and grain boundries from thirty one (31) Mobil Tyco silicon sample numbers 47 to 77 are also discussed.

A brief review of the changes made to upgrade the Quantimet 720 Image Analysis System is included in this report.

#### SECTION II

### INTRODUCTION

The objective of this program is to evaluate and, if possible, predict conversion efficiency for a variety of silicon samples with differences in structural defects, such as grain boundaries, twin boundaries, precipitate particles, dislocations, etc. Quantitative characterization of these structural defects, which have been revealed by etching the surface of silicon samples, can then be performed by using a Quantimet 720 Image Analyzer.

The silicon samples have been obtained by JPL from different manufacturers. Each of these manufacturers use their own crystal growth and fabrication techniques and, therefore, the various types of silicon produced contain a variety of trace impurity elements and structural defects. The two most important criteria in evaluating the various silicon types for solar cell applications are: (i) cost and (ii) conversion efficiency. At present, the solar cells with highest conversion efficiency are made of high purity silicon single crystals, which are free from structural defects such as dislocations, twin boundaries, precipitate particles, etc. But these single crystal solar cells are very expensive and may not meet the DOE goal of 50 cent/watt by 1986. On the other hand, silicon crystals such as EFG ribbons, Dendritic Webs, etc. are NOT single crystals but made of highly ordered crystals which contain large number of dislocations, twin boundaries, grain boundaries, precipitates, etc., compared to the premium grade silicon.

The following important questions must be answered to evaluate the conversion efficiency of low cost and high cost silicons: (i) What effect do these defects have on conversion efficiency of low cost and high cost silicons? (ii) Of the various types of defects, which defect/defects severely affects conversion efficiency? (iii) At what concentrations does this effect become significant? (iv) Is there a rapid, accurate, quantitative method that can be used routinely as a Quality Assurance tool?

Quantitative analysis of surface defects is being performed by using a Quantimet 720 Quantitative Image Analyzer. This sytem can differentiate and count 67 shades of gray levels between black and white contrasts. In addition, it can characterize structural defects by measuring their length, perimeter, area, density, spatial distribution, frequency distribution (in any preselected direction), and so on. However, the Quantitative Image Analyzer is extremely sensitive to optical contrasts of various defects. Therefore, to obtain reproducible results, the contrasts produced by various defects must be similar and uniform for each defect types along the entire surface area of samples to be analyzed. To achieve this, a chemical cleaning and polishing technique has now been perfected for silicon samples from Mobil Tyco, Wacker, IBM, and Motorola. The cleaning and polishing preparation technique produces a very clean and even surface for silicon crystals suitable for analyses by the QTM 720 Image Analyzer. We are now obtaining quantitative information from a variety of silicon crystals. Quantitative data on 31 Mobil Tyco samples are given in this report.

The Quantimet 720 Image Analyzer is now being upgraded with the addition of a P.D.P. 11/03 minicomputer (with dual floppy discs), a DIGITAL Equipment Corporation LA-120 high speed printer and a Field-Image-Feature Interface module (F.I.F.I.).

These changes will greatly enhance the speed and reliability of the Quantimet 720 system at no additional cost to JPL.

#### SECTION III

#### CHEMICAL POLISHING AND ETCHING OF MOTOROLA SAMPLES

#### CHEMICAL POLISHING:

In our previous Quarterly Report<sup>1</sup> and One-Time Report<sup>2</sup> on Crystal Cleaning and Polishing techniques, we have discussed in detail the procedures of chemical polishing and chemical etching. These techniques were perfected for Wacker, IBM, and Mobil Tyco samples. However, as mentioned in our Quarterly Report<sup>1</sup>, there is a variation in polishing time for the Wacker, Mobil Tyco, and IBM samples. This variation is due to certain inherent manufacturing, fabrication, and processing variables, which affect the chemical reaction rates for the three types of the samples under otherwise identical polishing conditions. Similarly, the polishing time of the silicon samples manufactured by Motorola has been observed to be different from those of IBM, Wacker, and Mobil Tyco samples.

The results of chemical polishing of Motorola samples are summarized in Table 1. It may be observed from the Table 1 that the polishing temperature of  $50^{\circ} \pm 3^{\circ}$ C and polishing time of 35-45 seconds are acceptable for the Motorola samples. However, the Wacker samples require 80-85 seconds, the IBM samples require 30 seconds, and the Mobil Tyco samples require 45 seconds for polishing.

It may be noted that samples which are slightly underpolished as well as samples which are well-polished, exhibit bright and shiny surfaces when observed by the naked eye. Therefore, visual observation cannot be used to determine the quality of polishing. However, when the samples are observed in a high quality optical metallograph, the underpolished samples

show faceting and sub-grain type structure, whereas the well-polished samples show clearly defined grain boundaries and some of the twin boundaries in sharp contrast. Therefore, an optical metallograph must be used to determine the quality of polishing.

## CHEMICAL ETCHING:

We have discussed in detail the composition and variation of the etching solution, the etching procedure, and the variation of the etching times in our previous reports  $^{1,2}$ . Etching solution III was used to distinctly reveal the strctural defects such as grain boundaries, twin boundaries, and dislocation pits for IBM, Wacker, and Mobil Tyco samples. This etching solution contained 10 g  $\rm C_r\rm O_3$  in 60 ml deionized water and 60 ml concentrated HF.

All the Mobil Tyco, IBM, and Motorola samples analyzed so far were etched for 50 seconds using etching solution III. The etching solution and etching time of 50 seconds were kept constant for all the samples. Since the samples were etched under identical conditions, the defects densities in these samples can be directly compared from one sample to another.

#### SECTION IV

#### TECHNICAL DISCUSSION

Chemical polishing and chemical etching of thirty one (31) Mobil Tyco samples and eight (8) Motorola samples were completed in the current reporting period. The 31 Mobil Tyco samples were then analyzed for twin boundaries, grain boundaries, and dislocation pits.

Procedure for QTM analysis, method of selecting fields, and explanation of teletype printouts are discussed below.

# Measurement of Twins and Dislocation Pits:

In the Mobil Tyco samples, almost all the twins are oriented parallel to one another and run from one edge of the wafer to the opposite edge (parallel to the longitudinal axis of the silicon ribbon). Therefore, in order to measure twin density, 50 fields were chosen along the central transverse axis of the sample. In other words, the central transverse axis is perpendicular to the twins. The distance between each of these 50 fields where measurements for twins were made was 0.31 mm. The long dimension of each field is 0.30 mm. Therefore, each of these fields are adjacent to one another by a distance of 0.01 mm, and therefore, do not overlap one another. It is important that the fields do not overlap, since the same twin should not be counted twice. At the same time, the fields must be close to one another so that almost all the twins are counted by the QTM. On the other hand, counting may also be done using a square raster of 50 fields distributed evenly over the entire sample surface. In this case, the horizontal distance separating each field will

be 2.5 mm, which is much larger than the long dimension of the frame i.e., 0.30 mm. Therefore, under the method of square raster, there is a possibility that areas in the sample where the twin or dislocation density is very high may not be counted. This will result in large errors. Therefore, all the 50 fields were counted along the central transverse axis of the sample.

It has also been found that the dislocation pit density in the Mobil Tyco samples have longitudinal symmetry similar to the twins<sup>1</sup>. Therefore, for the dislocation pit density measurements, all of the fifty fields were counted along the central transverse axis of the Mobil Tyco silicon samples.

# Measurement of Average Area of Twins and Dislocation Pits:

Before measurements were made for twins, each sample was scanned to determine manually the average area of one twin. The method of determining the average twin area is as follows: First, the sample surface was randomly scanned, and those fields were selected where the twins were not touching each other. Each field, generally containing more than 5 distinct twins, were then displayed on the display module of the QTM. The total area of all the twins in each field was determined and divided by the number of twins in that field to get the average twin area for that field. The average twin area was then determined in an additional 4 fields. The arithmetic average was then calcualted from the average twin area in these five fields. Generally, 30 to 40 twins are used in 5 fields to get the average twin area. The same procedure was used to obtain the average dislocation pit area. The average twin area in each sample was then fed into the Register (038) of the HP 9810. This is an important step to get actual number of twins and dislocation pits, especially in areas where the densities of

these defects are high and they touch one another. In order to verify that the average area of a twin so obtained was accurate, an additional six fields were selected at random where the twin density were high, and the twins were touching one another. The twin density in each of these six fields were counted manually, and also counted by the QTM using the average area of a twin. The entire procedure was repeated until close agreement was reached between manual counting and QTM counting. After this procedure, measurements were then made on all the 50 fields for each of the 31 Mobil Tyco samples using the automatic QTM mode.

# Explanation of Teletype Printout:

The QTM measurements for twins and dislocation pits on Mobil Tyco samples 47 to 77 are shown in attached teletype printouts. The first paragraph of the teletype printout gives the date, name of the manufacturer, sample number, name of the defect type being measured, size of the X and Y steps, and average values of twin area and dislocation pit area that were measured manually and fed into the Register 038 for each sample. In addition, the teletype printout for twin measurements also shows that the QTM output data is divided by 100. This procedure was followed in order to avoid frequent overflow problems in the Classifier-Collector.

The second paragraph of the teletype printout lists: 1) the 800 X magnification that was used; 2) calibrated equivalent value of one picture point in the units being used i.e. mm for twins and microns for dislocation pits; and 3) calculated area of one field (frame) in the units being used. The frame area of a standard frame in the QTM is 500,000 pictures points (pp). In case of twins, the standard frame was used. However, during dislocation density measurements the uneven sample surfaces caused problems

in focusing dislocation pits over the entire standard frame. Therefore, during dislocation density measurements half the standard frame (250,000 pp) was used. This is shown under "Frame Area" in the QTM data sheets. The unit of measurement was millimeter for twins, and microns for dislocation pits.

The third paragraph of the teletype printout lists the titles for the different measurements, which are explained below:

Field: indicates the sequence number of the field in which measurements were made.

No: denotes the total number of features detected in any field. This is obtained by dividing the total area of a feature by the average area of that feature.

No./Area: denotes the computed number of features/mm<sup>2</sup> or features/microns<sup>2</sup> in each field.

MFPV: denotes the mean free path in the vertical direction. This quantity is the frame area divided by the vertical projection of all detected features in the field (frame).

MFPH: denotes mean free path in the horizontal direction. This is the horizontal analogue of MFPV.

L/A: This quantity is length of detected features per unit area. The unit area is mm<sup>2</sup> in the case of twins and microns<sup>2</sup> in the case of dislocation pits.

Note: The quantity L/A is subject to large errors when twin bands are present. The QTM computes L/A by dividing the perimeter by 2. A twin band usually contains 20 to 100 individual twins, many of them touching

one another. The QTM will compute L/A by dividing the perimeter of the twin band by 2. In other words, the QTM may count the entire twin band as one large area rather than consisting of several individual twins. Thus, L/A is subject to large errors and is underestimated by QTM.

AFETA: This denotes the average area of the features detected in each field. This is to be ignored in the attached teletype printouts, since the average area was determined manually at the start.

Note: The attached teletype printouts show, after 25 and 50 fields, the computed values of average, standard deviation, and standard error for all data from field No. 1 onwards. This averaging can be done at any time during the course of the measurement.

For all the samples (Mobil Tyco 47 to 77), the average twin area was divided by 100 before feeding into Register 038 of the HP 9810. Therefore, the QTM data for "No." and "No./Area" are actual. However, 'MFPV" and 'MFPH" are to be divided by 100 (because "area" is the numerator and "intercept distance" is the denominator); and "L/A" is to be multiplied by 100 to obtain actual values.

The grain boundaries in each sample were counted under the binocular microscope using 7X magnification. Most of the grain boundaries were parallel or approximately parallel to the twins. In general, there were no complete grains in a sample, i.e., the grain boundaries were running from bottom edge to top edge of a sample.

# Upgrading of the Quantimet 720 Image Analyzer:

During the month of February, the Quantimet Image Analyzer system (QTM 720) was upgraded with the addition of a PDP 11/03 minicomputer, a Field-Image Interface Module (F.I.F.I.), and a DIGITAL Equipment LA-120 teletype. These modifications will result in a significantly improved image analysis system at no additional cost to JPL.

The PDP 11/03 minicomputer, that replaces a Hewlett-Packard Model 9810 desk top calculator, has a dual floppy disk drive and 64K bytes of memory. This new system allows software control of most Quantimet 720 data acquisition and analysis functions. These functions include the X, Y specimen stage motion (with automatic focusing), variable frame position, gray level detection, and feature measurements such as area, perimeter, vertical projection, and horizontal projection.

The link between the PDP 11/03 minicomputer and the Quantimet 720 Image Analyzer is the Field-Image-Feature Interface module<sup>3</sup>. This new module allows feature specific data acquisition, which was not possible on the earlier system. This module transfers data on image fields or on individual features to the computer core memory at very high speed. Geometric, densitometric, and co-ordinate data can be transferred from the Quantimet 720 to the PDP 11/03 minicomputer. Data for all the features in the field may be transferred, or data for only those features selected by the Quantimet size discrimination; or data selected by the image editor may be transferred to PDP 11/03. Pattern recognition can be performed by the PDP 11/03 using shape functions derived from feature measurements.

The results of this pattern recognition can be used to define automatically the region for full image transfer. Also, with this system a computer generated digitised image and a complete character format can be superimposed on the Quantimet 720 display screen<sup>3</sup>. Real time updated histograms, labels on features that satisfy preprogrammed pattern recognition tests, and numerical measurements on selected features can be displayed.

This system allows for very flexible data acquisition and analysis. Since the PDP 11/03 software controls many of the functions of the Quantimet 720, there is less chance for operator error. The time required to scan and analyze a field is now about 5 seconds as compared with about 10 seconds for the earlier system.

Data is recorded on floppy discs. Each disc can record the data from about 80 silicon samples (50 fields per sample). The data is output on a DIGITAL LA-120 Decwriter III printer which replaces a teletype. The LA-120 has a printing rate of 180 characters per second, which is a great improvement over the earlier teletype that had a printing rate of 10 characters a second. The addition of the LA-120 printer and floppy disc data storage system makes a significantly improved data storage and retrieval system.

The F.I.F.I. module allows for feature specific area scans. This additional capability will have to be investigated in order to determine if it can be advantageously applied to the analysis of defects in silicon samples.

This new equipment should become operational sometime in May, but additional time will be required for personnel to learn to operate the new system. Also, a new computer program must be written for the PDP 11/03 minicomputer that will co-ordinate the data acquisition and analysis functions of the Quantimet 720.

#### SECTION V

## RESULTS

Sixty two (62) teletype printouts containing data on thirty one (31) Mobil Tyco samples are attached herein. For each sample, there are two teletype printouts, listing data separately for twins and dislocation pits. In addition to the teletype printouts; data on twins, dislocation pits, and grain boundaries have been summarized in Tables 2 to 5 for ease of correlation and comparison. Each table contains data from eight specimens cut from the same ribbon (see Fig. 1).

Grain boundary length/cm<sup>2</sup> have been measured and computed for each sample using a binocular microscope at a magnification of 7X.

There is no clear cut relationship present between twins, grain boundaries and dislocation pits among these samples whether cut from the same ribbon or when samples from different ribbons are compared.

Specimens from ribbon 5-640 MRR #1 contain lowest density of twins/mm<sup>2</sup> when compared with specimens cut from ribbons 5-640 MRR #2, 5-745, and 5-743. Similarly, specimens from ribbon 5-640 MRR #2 show lowest density of dislocation pits when compared to specimens from other ribbons. In general, the twin and dislocation densities in specimens taken from ribbons 5-640 MRR #1 and #2 are comparable. Similarly, the twin and dislocation densities in specimens from ribbon 5-745 and 5-743 are comparable. Specimens from these two ribbons on the whole exhibit higher densities of twins and dislocations when compared with specimens from ribbons 5-640 MRR #1 and #2.

Polishing time of the Motorola samples has been found to be 35-45 seconds using a temperature of  $50^{\circ}\text{C} \pm 3^{\circ}\text{C}$ . The etching solution and etching time of 50 seconds were kept constant for all of the samples. Since the samples were etched under identical conditions, the defect density in the samples can be directly compared.

#### SECTION VI

### CONCLUSIONS

Polishing and etching procedures have been perfected for Mobil Tyco, Wacker, IBM, and Motorola silicon samples for obtaining proper contrast of structural defects suitable for QTM analyses.

A computer program for automated quantitative image analyses of grain boundaries, twin boundaries, and dislocation pits using a Quantimet 720 Image Analyzer has been perfected and is being used routinely.

Data collected on thirty one (31) Mobil Tyco samples using the Quantimet 720 Image Analyzer is discussed.

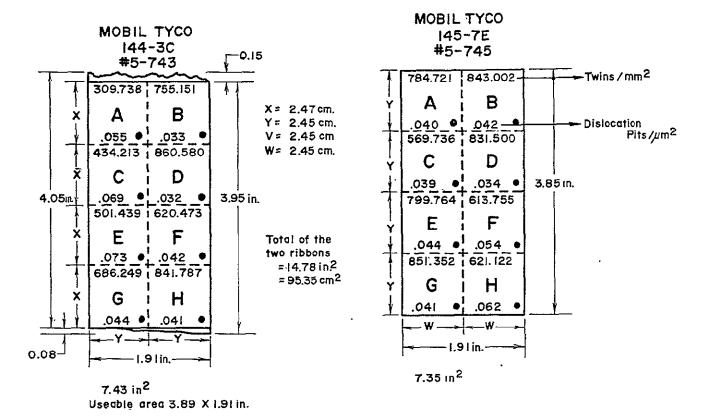
After the thirty one (31) Mobil Tyco samples were analyzed, the Quantimet 720 Image Analyzer system was upgraded with the addition of a PDP 11/03 minicomputer (with dual floppy disc drive), a Field-Image-Feature-Interface module, and a DIGITAL Equipment Corporation LA-120 high speed printer.

These changes will result in a much improved data storage and retrieval system, and should increase the speed and reliability of the Quantimet 720 system.

#### SECTION VII

# REFERENCES

- 1. R. Natesh, J. M. Smith, H. A. Qidwai: "Quantitative Analysis of Defects in Silicon," Quarterly Progress Report No. 3, DOE/JPL 954977, Materials Research, Inc., Technical Report: MRI-264, 1979.
- 2. R. Natesh, H. A. Qidwai: "Quantitative Analysis of Defects in Silicon," One-Time Report on Crystal Etching Preparation Technique, DOE/JPL 954977, Materials Research Inc., Technical Report: MRI-259, 1978.
- 3. Quantimet 720 Image Analysing Computer Operating Manual, 2nd Edition, Cambridge Instrument Company, Inc., November, 1971.



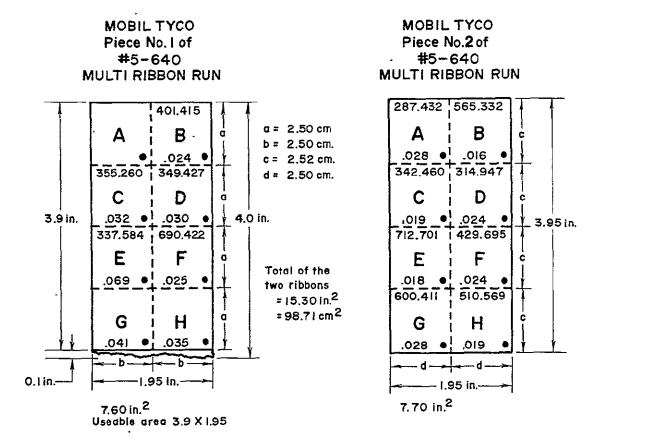


Fig. 1. Schematic sketch showing location of 32 Mobil Tyco samples from four ribbons. In each square (representing a sample), the number at top represents average twin density/mm<sup>2</sup> and the number at bottom represents dislocation density/microns<sup>2</sup>. 24

TABLE 1

CHEMICAL POLISHING OF MOTOROLA SAMPLES

Polishing solution: mixture of  $HNO_3:HF:CH_3COOH = 1:2:3$  by volume

Temperature (°C)	Time (Sec.)	Surface Condition
50	30	Growth lines persist. Sub-grain type structures present
50	35-45	Good even polishing
50	50	Faceting develops

T A B L E 2

ANALYSIS OF MOBIL TYCO SAMPLES

MRI Sample #	JPL Sample #	No. of Twins/field	No. of 2 Twins/mm <sup>2</sup>	Grain boundary length/cm <sup>2</sup>	No. of Dislocation Pits/field	No. of Dislocation Pits/µm²
47	5-745 A	21.78	309.738	0.72	1949.83	0.055
48	5-745 B	53.10	755.151	1.93	1166.29	0.033
49	5-745 C	30.53	434.213	1.82	2428.95	0.069
50	5-745 D	60.51	860.580	3.44	1122.38	0.032
51	5-745 E	32.26	501.439	3.31	2583.40	0.073
52	5-745 F	43.63	620.473	2.30	1493.01	0.042
53	5-745 G	48.25	686.249	2.00	1556.36	0.044
54	5-745 H	59.19	841.787	1.84	1434.39	0.042
	· · · · · · · · · · · · · · · · · · ·					

TABLE 3

# ANALYSIS OF MOBIL TYCO SAMPLES

MRI Sample #	JPL Sample #	No. of Twins/field	No. of <sub>2</sub> Twins/mm <sup>2</sup>	Grain boundary length/cm <sup>2</sup>	No. of Dislocation Pits/field	No. of Dislocation Pits/µm
55	5-743 A	55.18	784.721	2.27	1423.18	0.040
56	5-743 B	59.27	843.002	0.94	1465.18	0.042
57	5-743 C	40.06	569.736	1.96	1376.75	0.039
58	5-743 D	. 61.62	831.500	2.00	1189,66	0.034
59	5-743 E	56.23	799.764	2.04	1532.03	0.044
60 .	5-743 F	43.17	613.955	2.72	1885.17	0.0 54
61	5-743 G	59.86	851.352	2.48	1458.14	0.041
62	5-743 Н	43.67	621.122	1.76	2190.90	0.062

TABLE 4

ANALYSIS OF MOBIL TYCO SAMPLES

MRI Sample #	JPL Sample #	No. of Twins/field	No. of 2 Twins/mm <sup>2</sup>	Grain boundary length/cm <sup>2</sup>	No. of Dislocation Pits/field	No. of Dislocation Pits/µm <sup>2</sup>
	(MRR #1)		•			
63	5-640 B	28.22	401.415	1.60	860.36	0.024
64	5-640 C	24.98	355.260	1.40	1136.35	0.032
65	5-640 D	24.57	349.427	2.52	1072.13	0.030
66	5-640 E	· 23 <b>.</b> 74	337.584	2.39	2427.54	0.069
67	5-640 F	48.55	690.422	2.19	860.34	0.025
68	5-640 G	18.67	265.506	1.08	1434.89	0.041
69	5-640 Н	45.92	653.085	0.59	1245.87	0.035

TABLE 5

ANALYSIS OF MOBIL TYCO SAMPLES

MRI Sample #	JPL Sample #	No. of Twins/field	No. of <sub>2</sub> Twins/mm <sup>2</sup>	Grain boundary 2 length/cm	No. of Dislocation Pits/field	No. of Dislocation Pits/um
	(MRR #2)					· ·
70	5-640 A	20.21	287.431	1.92	976.88	0.028
71	5-640 B	39.75	565.332	2.76	576.89	0.016
72	5-640 C	24.08	342.460	2.60	685.26	0.019
73	5-640 D	22.14	314.947	2.19	850.34	0.024
74	5-640 E	50.11	712.701	2.00	621.43	0.018
75	5-640 F	30.21	429,695	1.55	842.35	0.024
76	5-640 G	42.22	600.411	1.82	998.84	0.028
77	5-640 Н	35.90	510.569	2.35	650.94	0.019
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AVERAGE TWIN AREA 33-52X120

MAG-838-2 UNITS-MM CALL FACTOR

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SE       6.00       85.716.555555555       1.478       \$555555555         27       23.35       474.357       1.906       1.616       7.49       0.007031         28       77.36       1.00       1.550       1.150       3.933       1.909017         29       26.61       378.467       6.262       1.552       7.12       1.201037         37       1.5.13       21.5.165       1.2300       2.155       1.496       .019375         31       9.93       1.741.289       9.888       3.989       3.304       7.797116         32       56.71       806.577       3.488       1.752       3.645       3.390024         32       56.71       806.577       3.488       1.752       3.645       3.390024         32       56.71       806.577       3.488       1.752       3.645       3.390024         32       56.71       806.577       3.488       1.752       3.645       3.390024         32       56.71       806.577       3.488       1.272       3.933       1.970016         32       56.71       806.577       8.152       1.218       3.883       3.2900118         32       73.72
SE       6.00       85.716.555555555       1.478       \$55555555         27       33.35       374.357       3.906       1.616       1.749       0.993031         26       77.36       1.00.766       6.250       1.159       3.933       1.999017         29       26.61       378.367       6.250       1.550       7.12       1.000007         37       1.5.13       215.165       1.2300       2.155       1.496       7.99307         31       9.93       1.741.289       9.888       3.989       3.334       7.297316         32       56.71       806.577       5.848       1.752       3.645       3.390024         32       56.71       806.577       5.848       1.752       3.645       3.390024         33       667.36       955.048       6.466       1.172       3.933       1.990018         34       63.39       901.618       8.152       1.258       7.845       7.990018         35       59.4       163.7       1.215       3.883       3.290019       3.790018         36       48.35       687.775       3.348       7.962       1.163       7.30019         37       72.55
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\$\frac{27}{23.35}\$ \frac{17.65}{27.36}\$ \frac{1}{29.35}\$ \frac{1}{25.55}\$ \frac{1}{29.35}\$ \frac{1}{25.55}\$
\$\frac{27}{23.35}\$ \frac{14.357}{1.0916}\$ \frac{1.616}{1.749}\$ \tag{0.997931}\$ \\ 28 \frac{77.36}{37.36}\$ \tag{1.90}{1.86}\$ \frac{6.250}{6.250}\$ \tag{1.159}\$ \\ 39 \frac{3.35}{3.091}\$ \tag{0.997931}\$ \\ 29 \frac{26.61}{26.61}\$ \tag{0.986}\$ \tag{0.2550}\$ \tag{1.159}\$ \\ 307 \tag{0.98731}\$ \\ 307 \tag{0.98731}\$ \\ 327 \tag{0.98731}\$ \\ 327 \tag{0.98731}\$ \\ 328 \tag{0.98731}\$ \\ 329 \tag{0.98731}\$ \\ 320 \tag{0.98731}\$ \\ 320 \tag{0.98731}\$ \\ 321 \tag{0.98731}\$ \\ 322 \tag{0.98731}\$ \\ 323 \tag{0.98731}\$ \\ 324 \tag{0.98731}\$ \\ 325 \tag{0.98731}\$ \\ 327 \tag{0.98731}\$ \\ 328 \tag{0.98731}\$ \\ 329 \tag{0.98731}\$ \\ 321 \tag{0.98731}\$ \\ 322 \tag{0.98731}\$ \\ 334 \tag{0.98731}\$ \\ 335 \tag{0.98731}\$ \\ 347 \tag{0.98731}\$ \\ 348 \tag{0.98731}\$ \\ 349 \tag{0.98731}\$ \\ 340 \tag{0.98731}\$ \\ 341 \tag{0.98731}\$ \\ 341 \tag{0.98731}\$ \\ 342 \tag{0.98731}\$ \\ 343 \tag{0.98731}\$ \\ 344 \tag{0.98731}\$ \\ 345 \tag{0.98731}\$ \\ 345 \tag{0.98731}\$ \\ 346 \tag{0.98731}\$ \\ 347 \tag{0.98731}\$ \\ 348 \tag{0.98731}\$ \\ 349 \tag{0.98731}\$ \\ 340 \tag{0.98731}\$ \\ 340 \tag{0.98731}\$ \\ 340 \tag{0.98731}\$ \\ 340 0.98731
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MOSIL TYCO SAMPLH # 48 JRL 3 145-7E 5-745 SPEC 3

DISLOCATION PITS ONLY

31 MM STEP SIZE

MEAS REMENT ALONG THE CENTER LINE OF THE SAMPLE

AVERAGE DISLOCATION FIT AREA = 5.29 PP

MAG-80070-UNITS-MICRONS TAL FACTOR

ERAME AREA 3.515625000 74

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SE       317.68       3.369       \$5555555       46.619       3.339       2.117378         26       783.19       3.269       3.729       46.619       3.339       2.117378         27       7261.13       3.265       12.811       1.604       9.175       6.46195         28       5.18       3.265       12.811       1.604       9.175       6.46195         29       29.87       3.001       2.80.23       2.69.37       3.002       1.481257         30       65.78       3.32       2.46.979       669.63       3.002       2.90.597         31       292.78       3.36.38       24.574       22.9855       3.737       37.37         32       4.31.12       2.90.537       22.9855       3.737       3.72       2.90.537         33       1.34.59       3.004       1.29.132       1.24.785       3.73.506       3.005       1.589286         34       9737       30.004       1.75.886       2.00.962       1.334.       2.92.7221
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MOBIL TYCO SAMPLE 7.57 JPL 4 145/7E 5-745 SPEC 0

DISLOCATION PITS ONLY

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26 2826 85 27 2972 46 28 253 33 29 364 44 39 257 59 31 275 93 34 1281 85 33 275 56 34 1281 85 35 266 67 36 146 85 37 167 59	7.7807 25.4 7.7807 216.5 7.037 216.5 7.037 225.1 7.038 168.5 7.038 168.5 7.399 27.3 7.484 27.8 7.336 57.5 7.386 7.5 7.386 7	62 27.531 52 27.531 52 29.593 14 21.8.531 42 212.104 11 168.311 72 25.524 12 49.525 13 49.525 13 49.525 13 49.525 13 49.525 13 49.525	9.0764 3.764 3.797 3.797 3.798 1.717 1.7669 2.7969 2.7975 3.798 1.7975 1.7975 1.7975	653393 •423669 •579857 •259593 •493243 •746512 •854259 •173668 •224677 •940294 •716132 •7193789 •339638
26 2826 85 27 2972 4f 28 253 33 29 364 44 38 275 93 32 3471 48 33 275 56 34 128 85 35 266 67 36 144 85	7.7807 25 2 0.057 36 3 0.057 216 3 0.037 216 3 0.037 216 3 0.030 26 3 0.030 26 3 0.030 27 3 0.030 27 3 0.030 27 3 0.030 20 3 0.030 20 3 0.030 20 3 0.030 20 3 0.030 20 3 0.030 3 0.030 20 3 0.030	62 27.531 52 27.531 52 29.593 14 218.531 81 212.194 11 168.311 72 22.645 12 28.645 13 49.525 68 189.912 13 49.813 13 49.813 14 16 49.8 13 13 49.8 13 13 49.8	9.006 9.064 9.059 9.019 9.019 1.054 1.069 1.069 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769	.423569 .579857 .267593 .493243 .746512 .654259 .173568 .224677 .927474 .7173789 .7173789
26 2826 85 27 2972 46 28 253 33 29 364 44 39 257 59 31 275 93 34 1281 85 33 275 56 34 1281 85 35 266 67 36 146 85 37 167 59	7.7807 25 2 0.057 36 3 0.057 216 3 0.037 216 3 0.037 216 3 0.030 26 3 0.030 26 3 0.030 27 3 0.030 27 3 0.030 27 3 0.030 20 3 0.030 20 3 0.030 20 3 0.030 20 3 0.030 20 3 0.030 3 0.030 20 3 0.030	62 27.531 52 27.531 52 29.593 14 218.531 81 212.194 11 168.311 72 22.645 12 28.645 13 49.525 68 189.912 13 49.813 13 49.813 14 16 49.8 13 13 49.8 13 13 49.8	9.006 9.064 9.059 9.019 9.019 1.054 1.069 1.069 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769	653397 .423569 .579557 .268593 .493243 .73658 .224677 .947414 .716172 .77538 .957235 .793446
26 2826 85 27 2972 4f 28 253 33 29 364 44 38 275 93 32 3471 48 33 275 56 34 128 85 35 266 67 36 146 85 37 167 17	7.980 25 2 0.057 36 3 0.057 216 3 0.037 216 3 0.037 26 3 0.037 26 3 0.037 26 3 0.038 168 3 0.038 199 4 0.038 199 4 0.038 199 4 0.038 198 6 0.035 298 5 0.035 298	62 524 093 62 27 591 58 29 593 14 21 8 531 81 127 378 42 212 194 11 168 911 72 29 645 12 29 645 13 189 918 67 196 498 28 113 174 16 498 18 18 18 18 18	9.006 9.064 9.059 9.019 9.019 1.054 1.069 1.069 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769 1.0769	653397 .423569 .579557 .263593 .493243 .73668 .224677 .94744 .716172 .71737P0 .339538 .957255 .79346 .79346 .253417
26 2826 85 27 2912 46 28 253 33 29 364 44 30 257 55 31 275 93 32 3471 48 33 2955 56 34 1281 85 35 266 67 36 146 85 37 275 93 40 939 56 41 482 96	7.7807 25.4 7.787 216.5 7.037 216.5 7.037 216.5 9.937 205.1 7.088 168.3 7.088 27.3 4.184 21.8 7.336 27.3 4.184 21.8 7.336 27.8 7.336 27.8 7.336 11.9 7.346 11.9 7.347 11.42 9 7.317 142 9 7.317 142 9 7.317 142 9 7.317 142 9	62 27 591 52 27 591 52 593 54 21 8 531 51 127 378 42 212 194 11 168 913 72 28 645 12 28 645 12 28 645 12 28 645 12 28 645 12 28 645 12 28 645 13 77 4 14 65 243 13 766 13 766	9.0764 3.764 3.757 3.757 3.769 3.769 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3	653397 .423569 .579557 .268593 .493243 .73658 .224677 .947414 .716172 .77538 .957235 .793446
26 2826 85 27 2912 46 28 253 33 29 364 44 38 275 93 32 3471 48 33 2955 56 34 1281 85 35 1266 67 36 1146 85 37 1861 59 38 197 197 197 49 397 56 41 42 96	7.7801 25.4 0.257 3.6 0.257 21.6 0.212 174.5 0.212 174.5 0.212 174.5 0.213 1.8 0.213 1.8 0.214 21.8 0.214	62 524 003 62 27 591 52 29 593 14 21 8 531 51 12 7 378 42 212 104 11 168 311 72 25 524 12 26 645 12 27 525 68 189 012 53 189 018 61 130 498 63 130 498 63 130 498 63 130 498 63 130 498	9.0764 3.764 3.757 3.757 3.769 3.769 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3.772 3	653397 .423569 .579557 .263593 .493243 .73668 .224677 .94744 .716172 .71737P0 .339538 .957255 .79346 .79346 .253417
26 2826 85 27 2912 46 28 253 33 29 364 44 38 275 93 32 3471 48 33 2955 56 34 1281 85 35 1266 67 36 1146 85 37 1861 59 38 187 187 187 187 39 37 38 187 187 39 37 38 187 39 37 38 187 39 37 38 38 38 38 38 38 38 38 38 38 38 38 38	7.7801 25.4 0.257 3.6 0.257 21.6 0.212 174.5 0.212 174.5 0.212 174.5 0.213 1.8 0.213 1.8 0.214 21.8 0.214	62 524 003 62 27 591 52 29 593 14 21 8 531 51 12 7 378 42 212 104 11 168 311 72 25 524 12 26 645 12 27 525 68 189 012 53 189 018 61 130 498 63 130 498 63 130 498 63 130 498 63 130 498	9.0764 9.764 9.797 9.797 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1.7075 1	653397 .423669 .579857 .269593 .493243 .746512 .854259 .173668 .224677 .940204 .716132 .7193326 .339538 .953255 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .763346 .773346 .773346 .773346 .773346 .773346 .773346 .773346 .773346 .773346 .773346 .773346 .773346 .773346 .77346 .77346 .77346 .77346 .77346 .77346 .77346 .77346 .77346 .77346 .77346 .77346 .77346 .77346 .77346 .77346 .77346 .77346 .77346 .77346 .77346 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .77446 .774
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MOBIL: TYCO SAMPLE # 51 JPL' # 145-7E 5-745 PEC'T'
TWINS ONLY
2TM OUTPUT. DATA DEVIDED BY 10%

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MOBIL TYCO SAMPLE # 51 JPL 1/45-75 S-745 SPEC 5

DISLOCATION PITS ONLY

31 MM STEP SIZE

MEASUREMENTS ALONG THE CENTER LINE OF THE SAMPLE ONLY

AVERAGE DISLOSATION FIT AREA = 5.1 PP

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DATE LYESTS

MOBIL TYCO SAMPLE # 53 JPL # 145-7E 1 -745 SPEC.6

TWINS ONLY

JTM DUTPJE DATA BEING DIVIDED BY 100

-31 MM STEP SIEE

MEASUREMENT ALONG THE GENIER LINE OF THE SAMPLE DNLY

AVERAGE TWIN AREA = 28.11 X100

MAG-800 0 UNITS MM CALL FACTOR - 10.003075 UNITS/PP

FRAME AREA - 0 0 00013

FIELD NO. NO. VATEA MMEPLY

PROPERTY AREA - 1.003028

1 2 8 40 131 151 1 155 1 826 1 440 7.003028

2 8 40 12 11 440 2 556 1 843 7.003028
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一起,"我们是这样的,但是我们的,我都不是你是这个我的,我就是一定是不是是,我们就是我的是我们的身体,但这一点,只是一个一个人,就是不是一个一个一个一个一个一
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DATE 1/16/79

MOBIL TYCO SAMPLE # 53 JPL # 145-72 5-745 SPEC G

DISLOCATION PITS ONLY

31 MM STEP SIZE

MEASUREMENT ALONG THE CENTER LINE OF THE SAMPLE ONLY

AVERAGE DISLOCATION PLT AREA =5.33 PP

MAG-800.3 JNITS-MICRONS CAL. FACTOR—

FRAME AREA—3.515625300 DA

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DISLOCATION PITS DNUY

31- MM STEP-STEE

MEASIREMENT ALONG THE CENTER: LINE OF THE SAMPLE THLY

WERAGE DISLOCATION PIT AREA = 3.34 PC

MAG-809 # UNITS - MICRONS CALL FACTOR - 1.345209 UNITS APRIL

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DATE 1/20/79MOBIL TYCO SAMPLE # 57 JPE 1 144-3C .45-743 SPEC.C

DISLOCATION PITS DNLY

31 MM SIEP-SIZE

MEASUREMENT ALONG THE CENTER LIVE JF THE SEMPLE

AVERAGE PIL AREA = 5.17 PP

MAG-800.0 JNLFS-MILRONS CAL FACTOR

FRAME AREA 3.515625000 044

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MOBIL TYCO SAMPLE # 58 JPL#144-3C #5-743 SPEC D

TWINS ONLY
OTM DUTPUT DIVIDED BY 100

1-31 MM STEP SIZE

MEASUREMENT ALONG THE CENTER LINE OF THE SAMPLE
AVERAGE TWIN AREA = 29-86-X 107

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CONTENTION OF THE TRANSPORT OF THE TRANS
DEMORIE TYCH TAMPLE # SR TRUTT LA4-3C #5-743 SPEC D
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VAS REMENT ALINE THE CENTER LINE IF THE SAMPLE
AMERICAGE THIN AREA = 33.25 X 199

MAG-893.1 INNIS-MM CAL. FACTOR\*
AMERICAGE THIN AREA = 33.25 X 199

MAG-893.1 INNIS-MM CAL. FACTOR\*
AMERICAGE THIN AREA = 33.25 X 199

FIELD NO: NO. AGES MERV MPPH LA FETA
LAST FIELD NO: AGES MERV MPPH LA FETA
LAST FIELD DELETED
AMERICAGE THIN AREA = 13.25 X 199

LAST FIELD NO: AGES MERV MPPH LA FETA
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30 3£ DATE 1/20/79

MOBIL FYOU #62 JPL #144-30 #5-743 JPEO F

DISLOCATIONS DYLY.

31 MM STEP SIEE

MEASUREMENT ALONG THE JENTER LINE IF THE SAMPLE

AVERAGE PIT AREA =: 5.85 PP

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FRAME AREA- 3.515625999 14
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MATE 1/29779

MOBIL TYCH SAMPLE # 62-UPL #144-30 #5-743, SPEC H

DISLOCATION PITS DNLY

2-31, MIN STEP SIZE

MEASUREMENT ALONG THE CENTER LINE OF THE SAMPLE

AVERAGE DISLOCATION PIT AREA = 5-22 PP

MAG-800-0 UNITS-PICRONS CAL FACTOR

FRAME AREA - 3. 115625200 34.

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TWINS ONLY
OTM: OTTPJT DATA DIVIDED BY 13141 MM STEP SIZE
MEASUREMENT ALONG THE CENTER LINE OF THE SAMPLE DALY
AVERAGE TWIN AREA - 29 ESY103

MAG-800-0 UNITS M-CAL FACTOR - 1003375 NITS/PP
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26 613 57 27 1685 31 28 746 33 29 963 13 31 882 84 32 446 73 33 489 59 34 280 82 35 623 47 36 594 69 37 954 90 38 831 84 39 278 98 42 15 31 41 44 69 42 177 18 43 1473 08 44 1357 76 45 461 63	# 317	7.394 7.198 7.1987 7.7.338 7.2.338 7.39.770 95.178 101.792 1.25.334 1.71.793 95.178 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773 1.21.773	321 321 321 322 322 322 322 322	281392 1.617873 1.849876 2.269678 1.345313 2.125691 1.637384 1.283591 2.786585 1.148688 2.239242 1.897649 1.492676 1.492676 1.492676 1.492676 1.492676 1.335321 1.991499 1.381895 1.977966
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26 613 67 27 1685 31 28 746 33 29 65 13 39 175 71 31 882 84 32 446 73 33 489 59 34 623 47 36 594 69 37 95 4 90 38 831 84 39 278 98 40 15 31 41 44 84 42 179 18 43 1473 02 44 1357 76 45 46 63 46 63 47 374 93	3174 27 453 3 354 27 827 3 354 27 827 3 354 57 886 3 36 373 3 3 5 6 73 3 3 6 3 73 3 3 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	7.39.4 7.198 7.198 7.2.338 7.2.338 7.2.338 7.1.792 1.25.334 1.7.792 1.25.334 1.7.793 95.178 1.21.793 95.178 1.21.793 1.21.816 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.343.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2.345.750 2	3.324 3.324 3.324 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321	281392 1 617878 1 849876 2 269678 1 345313 2 125631 2 637384 1 283531 3 786585 1 48688 2 239242 1 492676 1 492676 1 492676 1 355321 1 921499 1 381785 1 35784 1 35784 1 35786 2 586128 1 666344 1 37462
26 613 67 27 1685 31 28 746 33 29 65 13 31 822 64 32 446 73 33 489 59 34 282 82 35 623 47 36 594 69 37 95 4 90 38 831 84 39 278 98 42 15 31 41 441 84 42 179 18 43 1472 00 44 1357 76 45 461 63 46 673 27 47 374 90 48 600 10	317 87 453 3 354 27 827 3 354 27 827 3 354 57 84 459 3 305 336 373 3 305 71 784 3 305 125 518 3 305 178 237 3 308 125 679 3 308 125 679 3 308 36 734 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	7.39.4 31.198 37.535 72.338 739.778 101.792 125.334 171.793 95.178 121.753 63.995 119.816 63.995 119.816 63.935 119.816 2343.750 117.816 2343.750 117.816 2343.750 117.816 2343.750 117.816 236.723 236.723 236.723 236.723	3.321 3.324 3.324 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.	281392 1 617878 1 849876 2 269678 1 345313 2 125631 1 283531 3 786585 1 48688 2 239242 1 492676 1 492676 1 492676 1 355321 1 921499 1 381885 1 566344 1 37462 1 264335
26 613 57 27 1685 31 28 146 33 29 965 13 31 822 74 32 446 73 33 432 59 34 237 82 35 623 47 36 594 69 37 954 90 38 831 84 39 278 98 40 15 31 41 84 41 179 18 43 1473 00 44 1357 76 45 461 63 46 273 27 47 374 90 48 606 13 49 1421 32	3174 87,453 3.354 27,4827 3.354 27,4827 3.3627 57,986 3.305 73,784 3.305 71,784 3.305 125,518 3.305 178,232 3.305 178,232 3.307 125,679 3.308 83,631 3.308 23,4827 3.308 23,4827 3.308 23,4827 3.308 23,4827 3.308 23,4827 3.313 221 613 3.328 23,4827 3.317 92,338	7.394 7.395 77.535 77.535 77.535 77.535 77.535 79.178 101.792 125.334 171.793 121.753 121.753 123.816 123.816 123.816 123.816 123.816 123.816 123.816 123.816 123.816 123.816 123.816 123.816 123.816 123.816 123.816 123.816 123.816 123.816 123.816 123.816 123.816 123.816 123.816 123.816 123.816 123.816 124.816 125.916 126.717 126.717 126.717 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176 127.6176	3.324 3.324 3.324 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321 3.321	281392 1.617873 1.849876 2.269678 1.345313 2.125631 1.637384 1.28531 2.786585 1.148688 2.239242 1.492676 1.492676 1.492676 1.492676 1.335321 7.991499 1.351885 1.566344 1.666344 1.264335 1.773979
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27   51   43   2   301   997   10   1965   341   312   29   224   22   306   178   71   19   42   319   30   2117   14   30   160   31   184   36   183   371   353   31   243   371   30   307   307   308   307   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308   308	1.99292 1.134916 2.825847 2.731585 1.257184 1.257351 1.369243 4.359375 1.857955 1.857955 1.857955 1.877313 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.95312
27   51   43   2   321   997   30   1965   341   322   324   22   306   178   71   19   142   339   32   217   14   3   160   31   1844   36   183   371   365   341   375   38   243   577   38   39   64   31   32   377   38   377   38   377   38   377   38   377   38   377   38   377   38   377   38   377   38   377   38   377   38   377   38   377   38   377   38   377   38   377   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378   378	1.99292 1.134916 1.825847 2.731585 1.253184 1.25375 1.369243 1.369243 1.369243 1.369243 1.369243 1.369375 1.873313 2.953125 1.873313 2.953125 1.873313 2.953125 1.774978 1.774978 1.643716 1.653225
27   51   43   2   321   997   373   1965   341   312   29   224   22   3966   6178   71   19   142   319   32   217   14   3   168   31   184   36   183   375   39   217   14   3   168   31   184   36   183   374   375   39   31   243   577   39   307   188   3   39   34   3   3   3   3   3   3   3   3	1.99292 1.134916 2.825847 2.731585 1.257184 1.257351 1.369243 4.359375 1.857955 1.857955 1.857958 1.879313 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.95312
27   51   43   3   321   997   363   341   332   35   36   371   365   341   332   35   371   365   341   332   35   371   365   341   339   35   217   14   3   366   31   844   36   83   375   36   37   368   37   369   37   37   38   37   38   37   38   37   38   37   38   37   38   37   38   37   38   37   38   37   38   37   38   37   38   37   38   37   38   37   38   37   38   37   38   37   38   38	1.99292 1.134916 2.825847 2.731585 1.257351 1.369243 4.359375 1.857955 1.857955 1.857955 1.87313 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.9
27   51   43   3   321   997   363   341   332   324   32   324   32   324   32   32	1.99292 1.134916 2.825847 2.731585 1.257184 1.257351 1.369243 4.359375 1.857955 1.857955 1.879313 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.6163657 2.616365 1.6365 1.534697 2.516155
27   51   43   3   321   997   363   341   332   324   32   324   32   324   32   32	1.99292 1.134916 2.825847 2.731585 1.257184 1.257351 1.369243 4.359375 1.857955 1.857955 1.87313 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.93125 2.9
27   51   43   3   321   997   363   371   365   341   322   324   32   324   324   325   324   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325   325	1.99292 1.134916 2.825847 2.731585 1.257184 1.257351 1.369243 4.359375 1.857955 1.857955 1.879313 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.953125 2.6163657 2.616365 1.6365 1.534697 2.516155
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ORIGINAL PAGE IS

DATEL/22/79
MOBIL TYCO #74 JPL5-643 MRR#2 SPEC E
DISLOCATION PITS ONLY
9.31 MM STEP SIZE
MEASUREMENT ALONG THE CENTER LINE OF THE SAMPLE
AVERAGE PIT AREA. = 5-25 P
MAG-843-9 JANITS-MICRONS CAL FACTOR
FRAME AREA - 3-515625009 JANITS-MICRONS CAL FACTOR
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DATE 1/22/79

MOSIL TYCO #75 JPL 5-640 MRR#2 SPEC F

TYINS ONLY

THM JUTFUL DIVIDED BY 170

STA MM STEP SIZE

MZ4SIREMENT ALONG THECENTER LINE )F THE SAMPLE

AVERAGE TRIM, AREA = 31.37 X 190

WAG-800 T UNITS-MM CAL FACTOR
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23 89 31 32 33	16, 77 16, 79 18, 55 132, 56 295, 94 243,9, 33 97,4, 40 312,8, 20	0 30 0 10 0 10 0 10 1 10 1 00 1 00 1 00	12 32 143 143 143 143 143 143 143 153 153 153 153 153 153 153 153 153 15	21.30 . 682 3924 . 194 5514 - 176 582 . 298 248 . 674 29 . 994 29 . 223	1. 199 1. 199 1. 108 1. 108 1. 262 1. 033	2.973554 1.757813 4.369853 1.382828 2.512143 1.597274 2.826376
257	16 77 16 79 18 55 182 56 295 94 2439 38 974 40 3128 20	0 100 0 100 0 000 1 000 0 000 0 000 0 000 0 000	12	21.30 . 682 - 302 1 . 194 - 5514 - 176 - 582 - 298 - 248 . 674 - 29 . 994 - 29 . 223 - 29 . 223	1. 129 1. 129 1. 108 1. 108 1. 262 1. 576 1. 576	1.757813 2.757813 2.757813 2.752828 1.322828 1.537274 1.537274 1.826376 4.642288
257	16 77 16 79 18 55 182 56 295 94 2439 38 974 40 3128 20	0 100 0 100 0 100 1 100 0 100 0 100 1 100	1512389 1232 143 2840 155 282 155 282 155 282 155 282 155 281 281	21.30 . 682 - 392 4 . 194 - 5514 - 176 - 582 . 298 - 248 . 674 - 29 . 994 - 29 . 223 - 29 . 223 - 29 . 216 - 29 . 223 - 29 . 216 - 20 . 216	1. 799 1. 799 1. 708 1. 762 1. 937 1. 9376 3. 978	1.757813 2.757813 2.769853 1.392828 2.512143 1.597273 2.826776 4.642288 2.463286
257	182,56 182,56 295,94 243,93,40 312,823 41,65,31 41,65,31	0 100 0 100 0 000 0 0 000 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1512389 1232 143 2840 985 4359555 282 4156 282 4156 281 456 281 482 151 638	21.30. 682 3024. 194 5514-776 582-898 248-674 29. 994 29. 223 20-716 23. 395 43. 547 133. 547	1. 199 1. 199 1. 108 1. 162 1. 133 1. 137 1. 137 1. 142 1. 142 1. 142	1.757813 2.757813 2.769853 1.392828 2.512143 1.597273 2.826776 4.642288 2.463286
21 28 29 33 33 33 33 35 36 37	182,556 182,556 295,94 243,934 312,833 4165,31 4162,97	0 100 0 100 0 000 0 000 0 100 0 0 0 0	15123491 2232 143 2439 555 262 152 26 238 26 238 26 712 21 638 21 638	2130.582 3024.194 5514.716 582-298 248.674 29.994 29.23 29.23 29.354 29.354 29.354 29.354 29.354 29.354 29.354	1. 199 1. 199 1. 108 1. 108 1. 162 1. 137 1. 178 1. 178 1. 178 1. 178 1. 178 1. 178	1.757813 2.757813 2.769853 1.392828 2.512143 1.597273 2.826776 4.642988 2.463276 2.676411
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35 36 37 39 41	38 67 72 67 186 22 742 67 1934 44 413 56 1922 19 215 33 117 78 48 99 1278 29 4257 33 1278 29 4257 33	7 225 7 235 7 275 7 3 155 7 3 155 7 3 156 9 3	579 348 324 394 196 749 162 478 155 579 196 131 223 578 223 578 123 454 1174 156 5514 156 147 348 147 348 167 412	121 \$121 1644 737 1644 737 192 246 192 595 193 595 193 575 436 1471 436 1471 436 1471 4376 487 111 198	9.1 19.2 19.305 19.305 19.305 19.305 19.305 19.305 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306 19.306	1.916316 3.54526 3.764627 2.569964 2.643466 2.134437 1.724881 1.593892 3.761364 3.964286 1.681369 2.504924
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